



Implication of Atmospheric Wetness Levels on Corrosion at a Coating Defect during Accelerated Testing

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Background

- SERDP program to develop improved accelerated corrosion test
- Many accelerated environmental tests exist
 - Developed by applying reasonable environmental conditions and ensuring resultant corrosion damage of a test system is realistic: **may or may not “excite” specific operational failure modes in other systems**
- Approach to new accelerated corrosion test
 - Thoughtful consideration of appropriate sample design
 - Make use of scientific understanding of corrosion mechanisms to develop exposure test cycle parameters

Outline

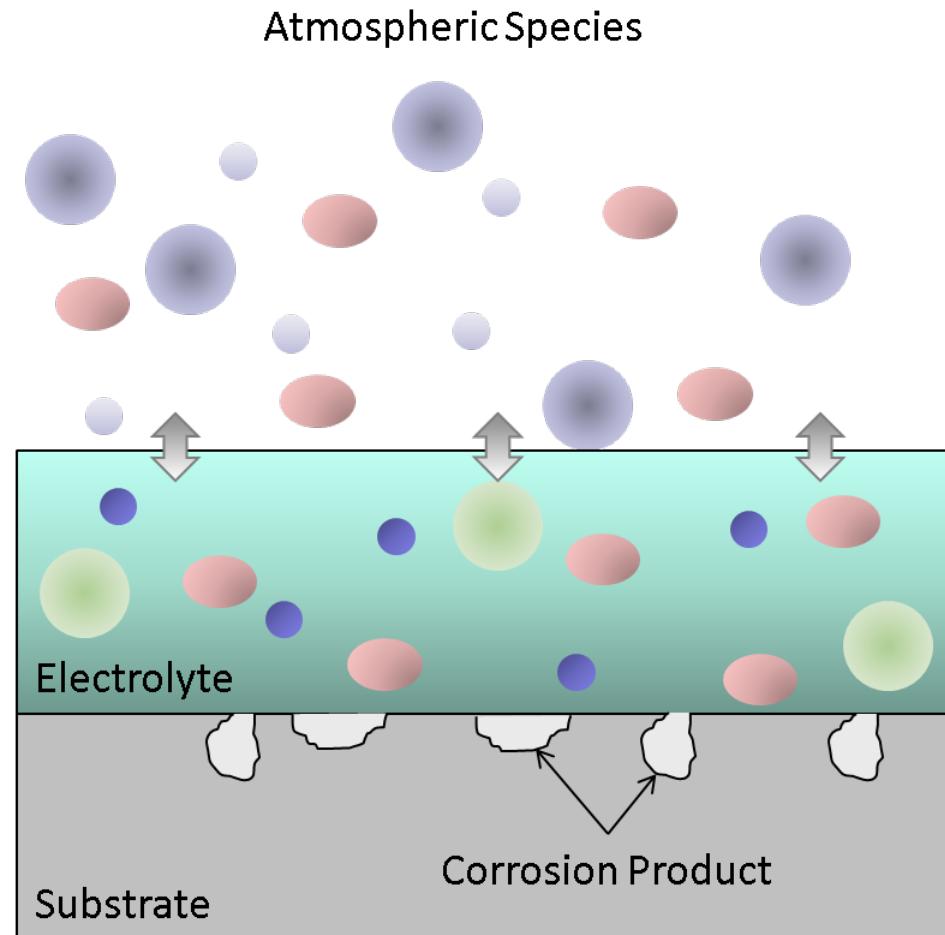
- Objectives
- Atmospheric corrosion
- Testing Approach
- Effect of RH on corrosion of steel
- Effect of inhibitor addition on coated steel
- Summary and future work

Technical Objective

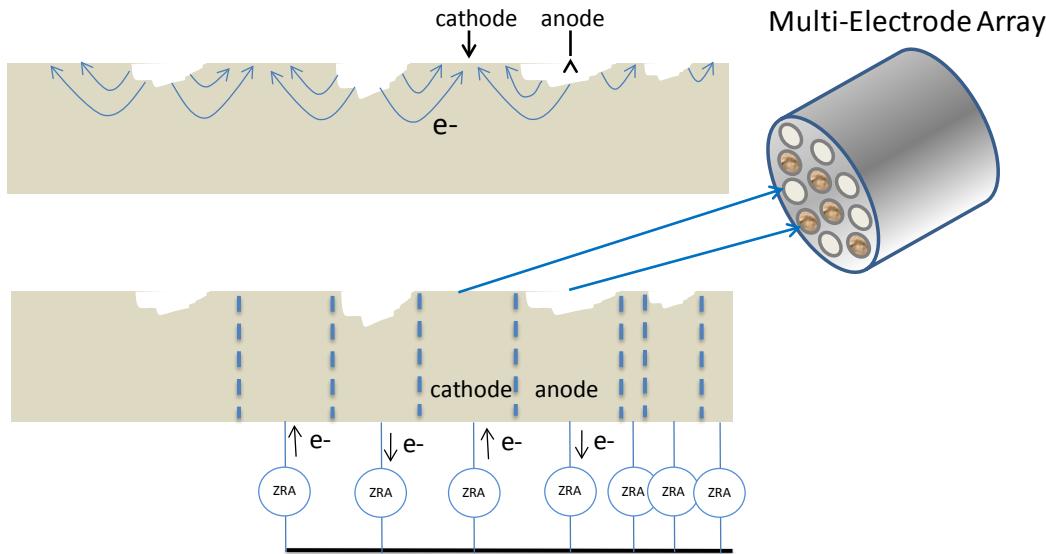
- **Objective**
 - Develop an understanding of how RH affect corrosion rate and perturbations in corrosion rate with inhibited coatings
- Why is understanding of RH effect important?
 - SAEJ2334 shows best correlations with field. Performed under wet bottom RH conditions (NOT FOG)
 - Cyclic conditions lead to different corrosion modes
 - SCC observed at salt deliquescence
 - Realistic conditions failure modes must be replicated in appropriate accelerated test methods

Atmospheric Corrosion

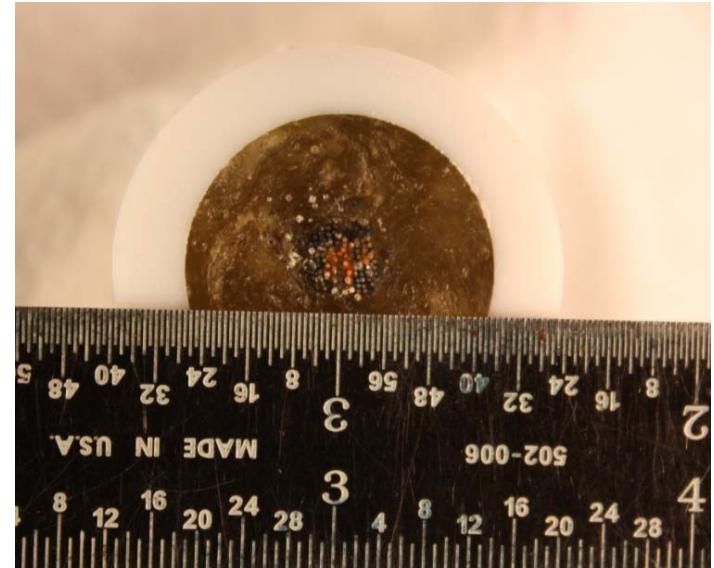
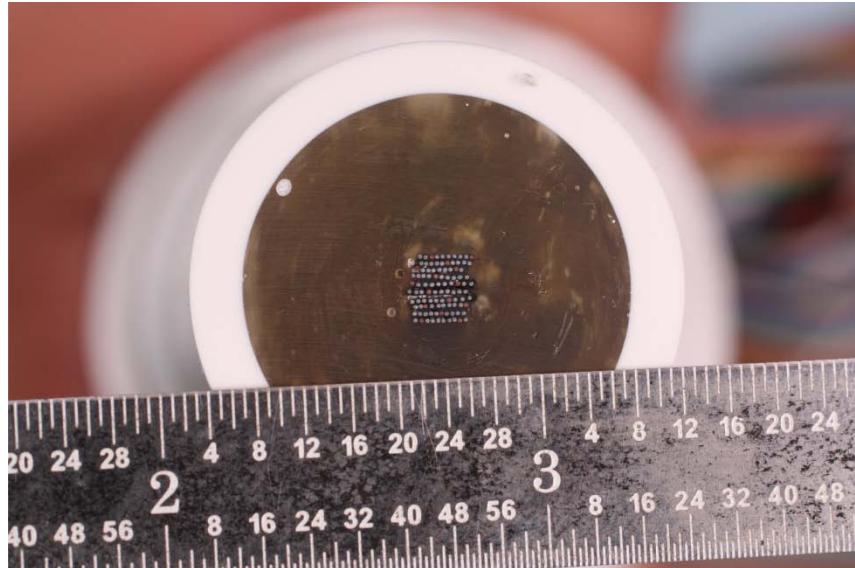
- Corrosion processes in the atmosphere are controlled by a thin film electrolyte layer on a metal substrate
- The electrolyte layer composition is controlled by
 - Atmospheric constituents (aerosols and gasses)
 - Relative Humidity (RH) and temperature
 - The presence of inhibitors in or galvanic interactions with coatings



Experimental Approach



- Corrosion (anodic site) and reduction (cathodic site) occur at the same rate
- Electrons flow from anode to cathode
- Multiple isolated anodes or cathodes develop
- Measure current at each electrode gives corrosion rate at the corrosion potential

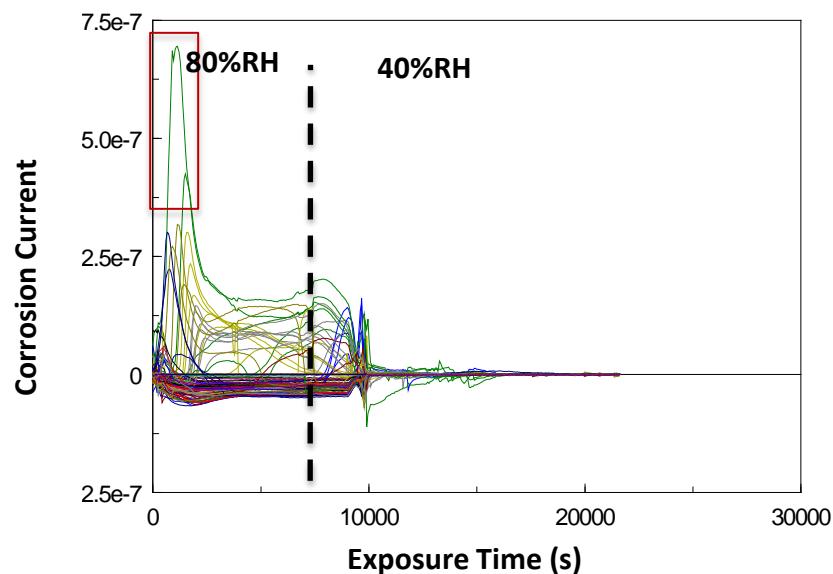


Experimental Procedure

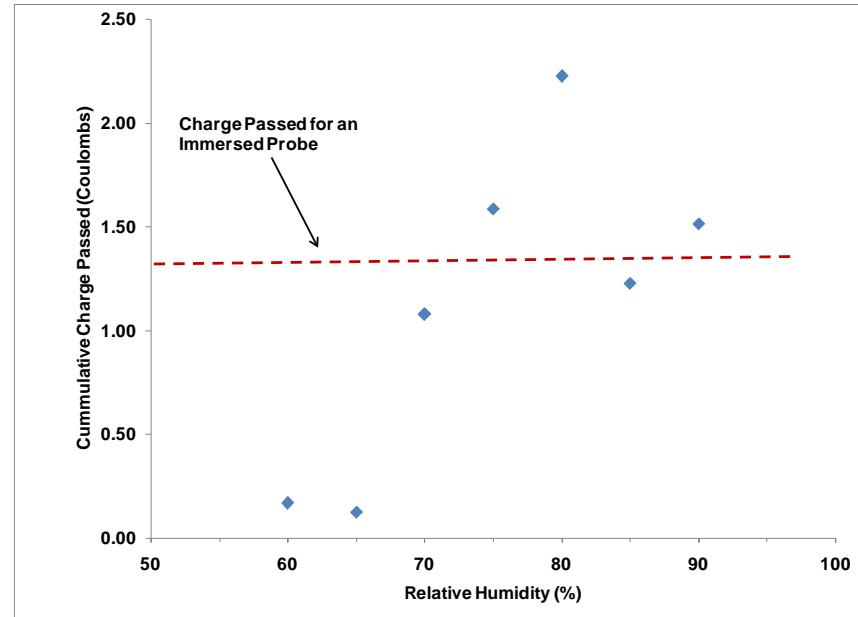
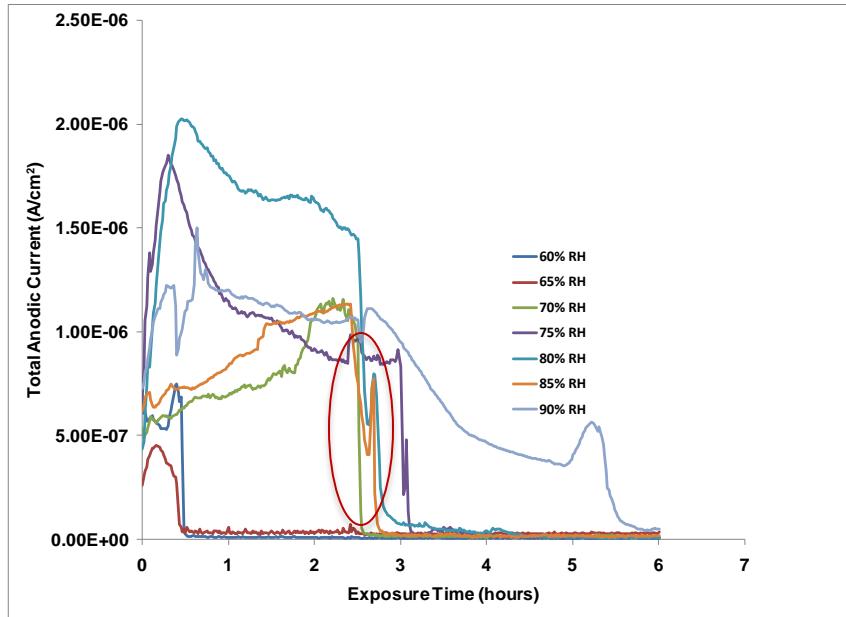
- 100 electrode (250 micron) multi-electrode probe fabricated using 1018 carbon steel
- $\sim 10\text{mg/cm}^2$ of NaCl placed over electrode elements (factor of 10 – 100 greater than outdoors)
- Atmospheric chamber used to control RH and temp
- Exposed under different RH conditions for 2.5 hour followed by reducing RH to 40%

Multi-Electrode Measurements

- chamber assembled to control iso-humidity conditions
- Anodic and cathodic regions form on multi-electrode probe



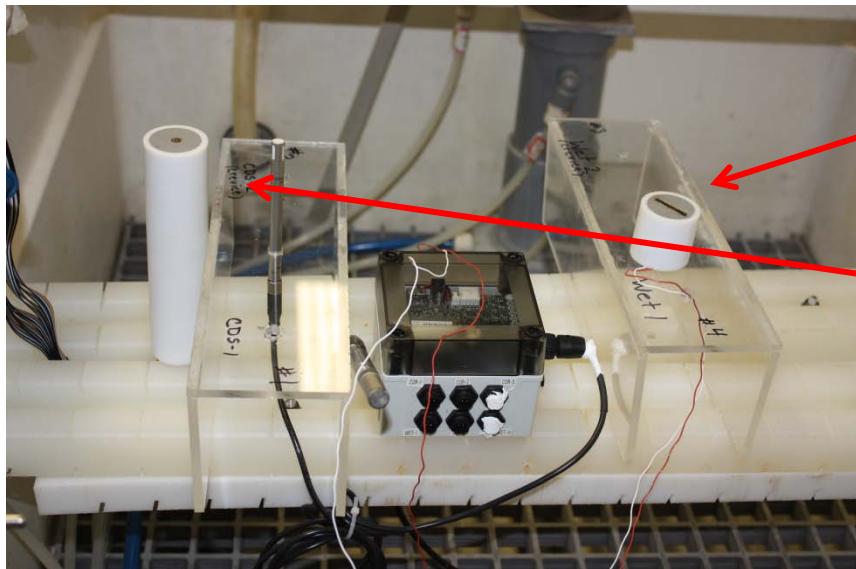
Measurements at Iso-Humidity



- Total anodic current vs. time shows different corrosion rates over time
 - < 70% is likely flash rust (short duration, electrolyte supports rust formation near 60% RH)
 - Anodic current peaks during wetting and drying
- Integration of current vs. time gives charge passed.
 - For NaCl covered surface and RH > 70%, , passed charge is similar to bulk liquid exposure

Measurements in Cyclic Humidity

- How does wetting and drying affect corrosion processes?
- Tests performed in an AutoTechnology accelerated corrosion test chamber
- RH cycled between high and low values. Temp = 30°C

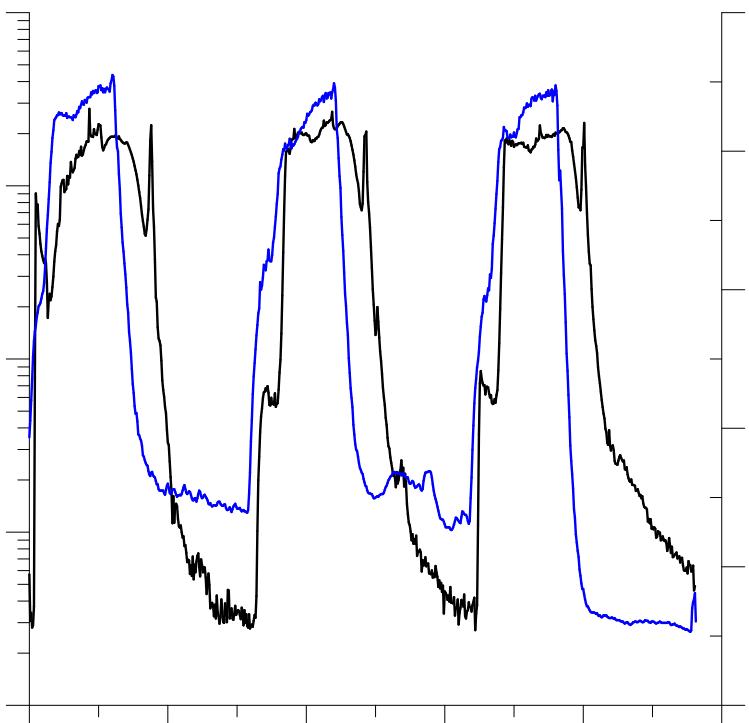


Parallel plate wetness probe



MMA and RH probes

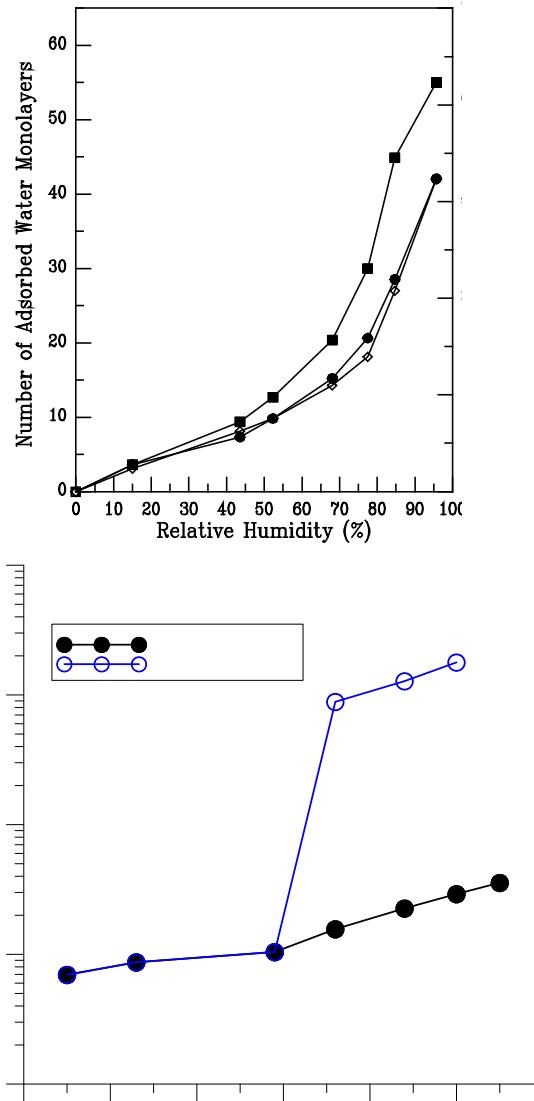
Measurements in Cyclic Humidity



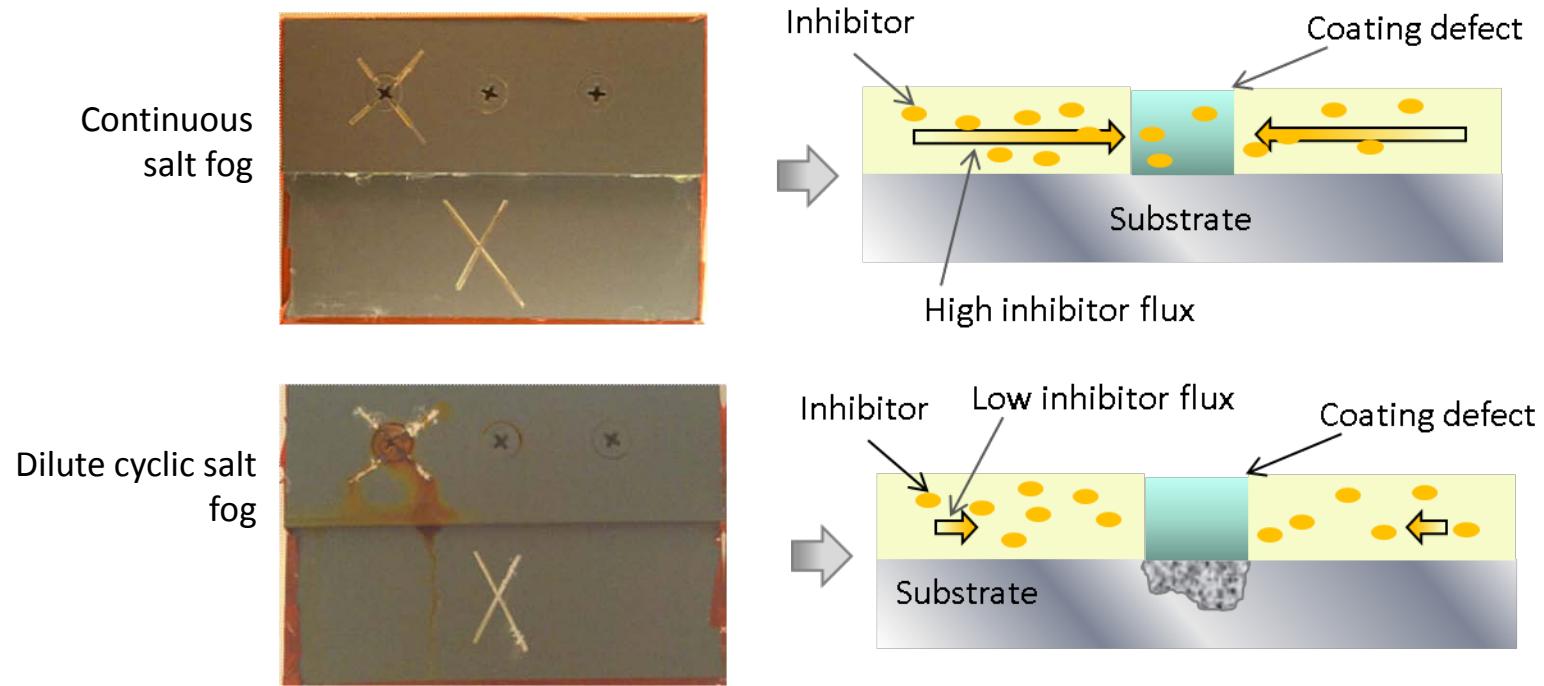
- Anodic current flows when RH is well below 40% and even as low as 15% during drying (efflorescence)
- Peaks in total anodic current are observed during wetting and drying
 - 60% - 65% = Thin film electrolyte behavior where initial high corrosion rate from oxygen availability followed by protective layer formation and decreasing corrosion rate
 - Above DRH = bulk electrolyte behavior + dissolved NaCl creating non-protective rust layer

Volume of Adsorbed Water

- Work by Dante and Kelly (1993) calculated adsorbed water onto Au
- Assuming Au and steel adsorption is similar and $30\text{ nl/cm}^2/\text{monolayer}$ of water, can calculate volume of adsorbed moisture with salt
- OLI calculations used to calculate volume of water with NaCl deliquescence
- Corrosion of Steel can occur at 60% RH, would expect some protection since NaCl is not dissolved
- Above DRH, bulk water accumulation so would expect non-protective oxide



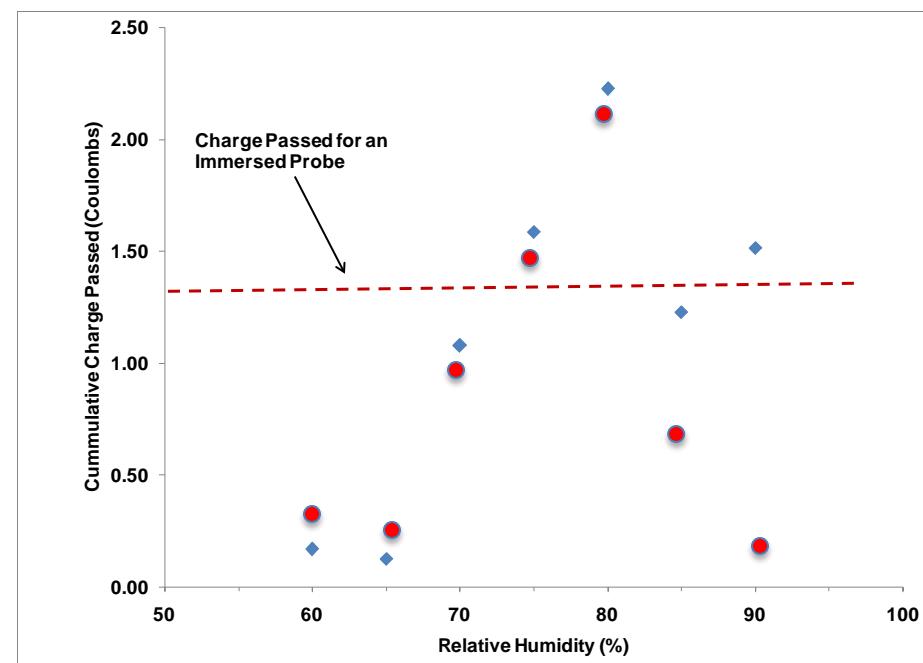
Hypothesis – Protection at a Scribe



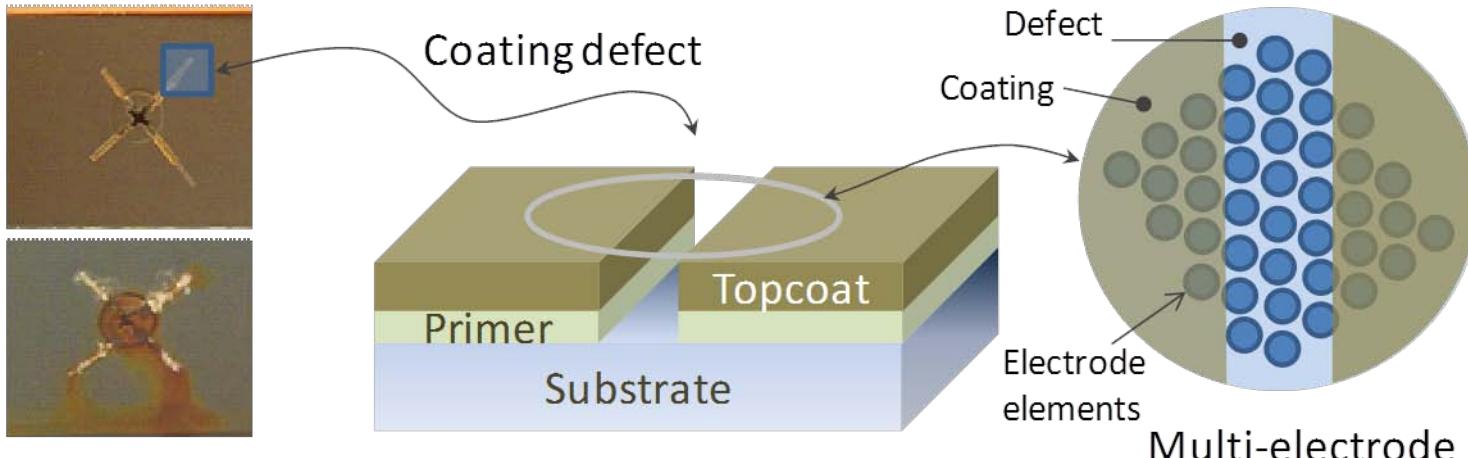
- Ability to protect substrate at a coating defect depends on connectivity between defect and mode of inhibition
- Moisture can promote inhibitor migration in the coating. For a given test method, wet and dry times will influence inhibitor mobility, and thus corrosion rate

Hypothesis – Protection at a Scribe

- For coated systems, what is the controlling process in corrosion failure at a scribe?
 - Corrosion rate of the substrate as a function of RH
 - Inhibitor mobility (or galvanic connectivity) (red dots are theoretical)



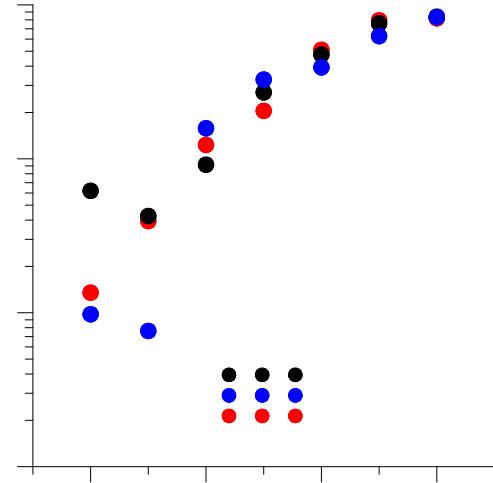
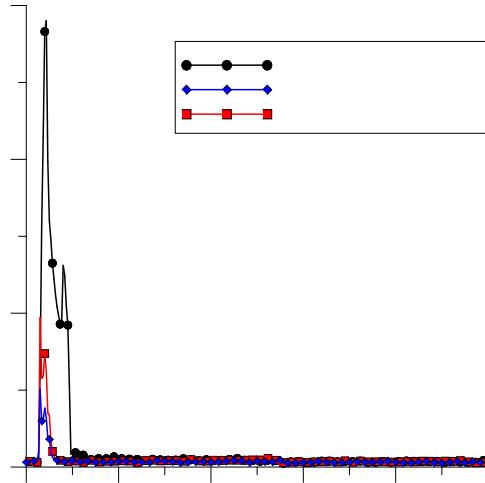
Simulation of Painted Surfaces



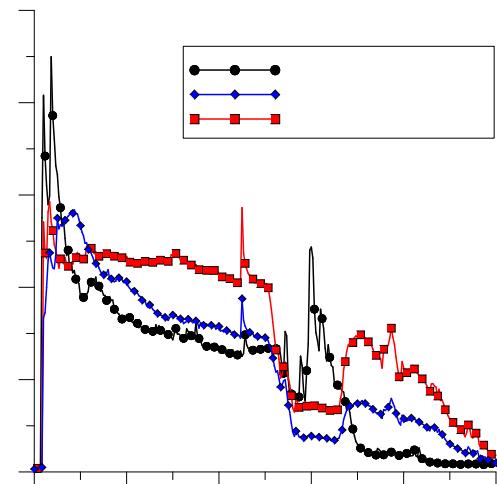
- Electrode surface painted leaving 20 electrodes (i.e. 2 rows) uncovered
- $\frac{1}{2}$ " o-ring placed over electrodes and salt deposited



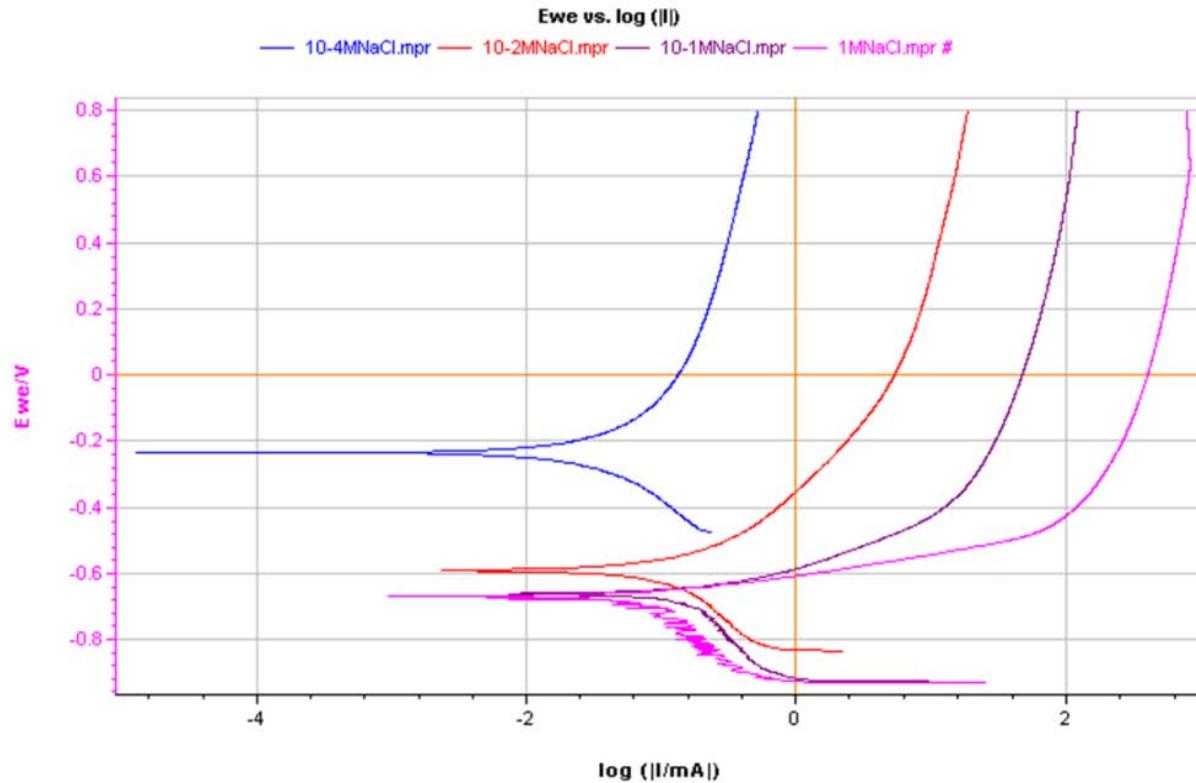
Effect of Inhibitor Leaching



- Inhibitors effect only below DRH
- Inhibitors suppresses the 60% RH peak for steel



Effect of Inhibitor Leaching



- Electrochemical potentiodynamic scans performed in $\text{NaCl} + 0.001 \text{ M NaCl}$ dichromate
- As NaCl decreases, cathodic current density increases
- Therefore, RH increases (NaCl decreases), total charge passed increases

Summary and Implications for Accelerated Testing

- Original hypothesis of chromate mobility decreasing with decreasing RH is not supported by the data
 - Component corrosion in cyclic environments controlled by galvanic interactions?
 - Need to determine what RH range results in decoupling of steel and aluminum
- Inhibitors protect against corrosion at 60% - 65% RH (flash rust) on steel
 - Short lived event that is likely inconsequential

Continuing Work

- Ongoing testing to define drying time as a function of
 - Time when RH > DRH
 - Drying time at differing RH values < DRH
- Testing using Aluminum electrodes